

$$\boxed{2-82.} \quad \omega_0 = 2\pi f_0 = 500 \Rightarrow f_0 = \frac{500}{2\pi}$$

$$f_s > 2f_0 = \frac{2(500)}{2\pi} = \frac{500}{\pi}$$

$$(a.) T_s = \frac{1}{f_s} \leq \frac{\pi}{500} = \underline{\underline{6.28 \text{ msec}}}$$

$$(b.) N = \frac{1 \text{ sec}}{6.28 \times 10^{-3} \text{ sec/sample}} = \underline{\underline{160 \text{ samples}}}$$

2-86.

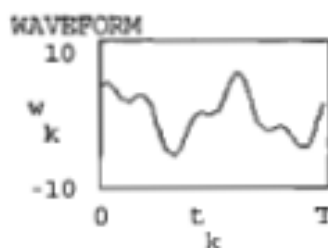
$$\begin{aligned}
 2-86 \quad & f_0 := 5 & \theta_1 & := 30 & T & := \frac{1}{f_0} \\
 & A_1 := 4 & f_1 & := 2 f_0 & \theta_2 & := -10 \\
 & A_2 := 2 & f_2 & := 5 f_0 & &
 \end{aligned}$$

$$\begin{aligned}
 M & := 5 & N & := 2^M & k & := 0 \dots N - 1 & T & := \frac{1}{f_0} \\
 dt & := \frac{T}{N} & t_k & := k dt & & & &
 \end{aligned}$$

$$w_{1k} := A_1 \sin \left[2 \pi f_1 t_k + \left[\frac{\pi}{180} \theta_1 \right] \right] \quad w_{2k} := A_2 \cos \left[2 \pi f_2 t_k + \left[\frac{\pi}{180} \theta_2 \right] \right]$$

$$w_k := w_{1k} + w_{2k}$$

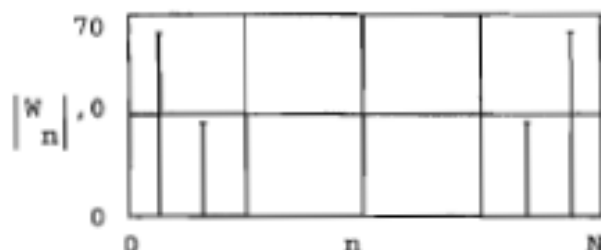
$$w_0 = 3.97 \quad dt = 0.006$$



Compute the FFT data points.

$$\begin{aligned}
 n & := 0 \dots N - 1 \\
 W & := \sqrt{N} \text{icfft}(w)
 \end{aligned}$$

FFT Data Points



$$n := \frac{-N}{2}, \frac{-N}{2} + 1, \dots, \frac{N}{2}$$

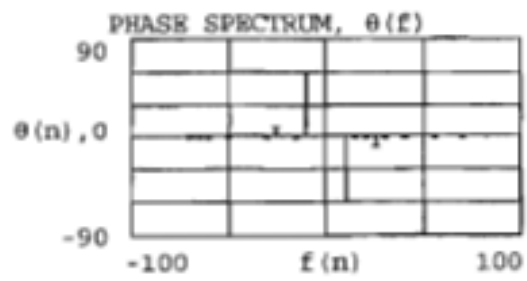
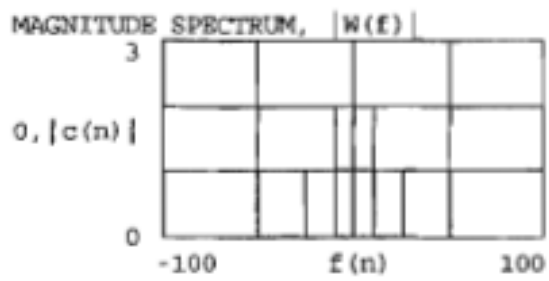
Since the waveform is periodic, the spectrum will contain only delta functions. ==> Evaluate the weights of the delta functions by using the FFT to calculate the complex Fourier series coefficients.
 =====> Use (2-187) and (2-178) along with (2-109).

$$c(n) := \text{if} \left[n \geq 0, \frac{1}{N} W_n, -\frac{1}{N} W_{N+n} \right] \quad f(n) := \frac{n}{T} \quad fs := \frac{1}{dt}$$

$$\theta(n) := \left[\frac{180}{\pi} \right] \arg(c(n) + 0.001)$$

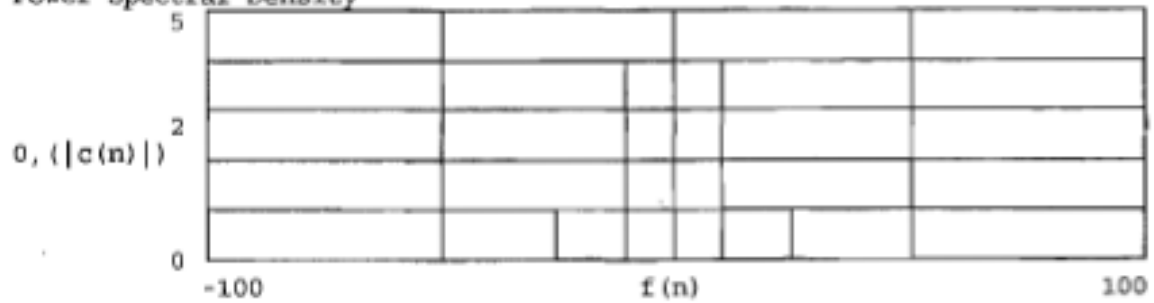
2-86 Cont'd.

(a) See next screen for a plot of the magnitude and phase spectrum.



(b) Use (2-126) to get PSD

Power Spectral Density



2-89

$$H(f) = \frac{1}{1+j(f/f_1)} \text{ where } f_1 = \frac{1}{2\pi RC} = B_{3dB}$$

Since $|H(f)|^2 = \left| \frac{1}{1+j} \right|^2 = \frac{1}{2}$, f_1 is the 3dB bandwidth.

$$(a) B_{eq} = \frac{1}{|H(f_0)|^2} \int_0^{\infty} |H(f)|^2 df = \int_0^{\infty} \frac{1}{1+(f/f_1)^2} df$$

$$= \int_0^{\infty} \frac{1}{1+x^2} (f_1 dx) = f_1 \tan^{-1}(x) \Big|_0^{\infty} = f_1 \frac{\pi}{2}$$

$$\left(\text{Let } x = f/f_1 \Rightarrow dx = (1/f_1) df \right)$$

$$\Rightarrow \underline{B_{eq} = \frac{\pi}{2} B_{3dB} = \frac{1}{4RC}}$$

(b.) Since $|H(f)| = 0$ only as $f \rightarrow \pm\infty$, the null bandwidth is ∞ . In this case the null bandwidth definition does not give a very useful measure of bandwidth because all RC low-pass filters will have $B_{null} = \infty$ regardless of the value of RC.

(c.) Answer is same as for Part (b.) above.

2-92. $s(t) = \Lambda\left(\frac{t}{T_0}\right) \leftrightarrow S(f) = T_0 [S_a(\pi f T_0)]^2$
↑
Table 2-2

(a) Using results in 2-61 (1.) above $\Rightarrow \underline{\underline{B_{dB} = \infty}}$

(b.) $S(f_{3dB}) = \frac{T_0}{\sqrt{2}} = T_0 [S_a(\pi f_{3dB} T_0)]^2$

$\Rightarrow \pi f_{3dB} T_0 \approx (2)^{1/4} \Rightarrow \underline{\underline{B_{3dB} = f_{3dB} = \frac{1.19}{\pi T_0} = 0.38/T_0}}$

(c.) $B_{eq} = \frac{1}{|H(f_0)|^2} \int |H(f)|^2 df = \frac{1}{T_0^2} \int T_0^2 [S_a(\pi f T_0)]^4 df$
 $= \frac{1}{\pi T_0} \left(\frac{\pi}{3}\right) = \frac{1}{3T_0} \Rightarrow \underline{\underline{B_{eq} = \frac{1}{3T_0}}}$

(d.) $B_{2\text{ rms cases}} = \frac{1}{T_0}$ (Similar to 2-90(4) above)